

GUIDELESS STAGE WITH ISOLATED REACTION STAGE

Field of Invention

5 The present invention relates, in general, to electro-mechanical alignment and isolation and, more particularly, to such method and apparatus for supporting and aligning a wafer in a microlithographic system and isolating the system from its own reaction forces and external vibrations.

Background of the Invention

10 Various support and positioning structures are known for use in microlithographic instruments. Typically, in the prior art, XY guides, including a separate X guide assembly and Y guide assembly, are utilized with one guide assembly mounted on and movable with the other guide assembly. Often, a separate wafer stage is mounted on top of these guide assemblies. These
15 structures require high precision and many parts. Typically, external forces directed to parts of the positioning assembly and reaction forces due to movement of different parts of the assembly are coupled directly to the image forming optics and reticle handling equipment resulting in unwanted vibration.

20 U.S. Patent 5,120,036 to Van Engelen et al. describes a two-step positioning device using Lorentz forces and a static gas bearing for an opto-lithographic device.

25 U.S. Patent 4,952,858 is directed to a microlithographic apparatus utilizing electro-magnetic alignment apparatus including a monolithic stage, a sub-stage and isolated reference structure in which force actuators imposed between the monolithic stage and the sub-stage are used for suspending and positioning

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Summary of the Invention

Broadly stated, the present invention is directed to method and apparatus utilizing a guideless stage for supporting an article and incorporating a reaction frame which isolates both
5 external forces as well as reaction forces created in moving the object from other elements of the system such as a lens system which produces an image that is exposed on the photoresist of a wafer object surface.

The present invention incorporates an object stage, a
10 reaction frame mounted on a base and substantially free from transferring vibrations between itself and the object stage, means for supporting the object stage in space independent of the reaction frame and cooperating force type linear actuator means mounted on the object stage and the reaction frame for
15 positioning of the object stage. The object stage can be mounted for movement in a given direction or can constitute a XY stage for movement in the X and Y directions while being supported in space in the Z direction.

A feature, an advantage of this invention is the provision
20 of a support, positioning and isolation assembly which allows the positioning function of the object or wafer stage to be accomplished while minimizing vibrations coupled to the stage and lens systems from the reaction stage faster and with fewer parts while minimizing vibrations coupled to the stage and isolating
25 the stage from undesired reaction forces.

In accordance with another aspect of the present invention, a positioning method and apparatus are provided for an XY stage with an independently moveable X follower and independently
30 moveable Y follower and cooperating linear force actuators mounted between the stage and followers whereby the movement of either follower does not effect the movement of the other follower.

Another aspect of this invention is the provision on at least one follower of a pair of arms on the follower with each

arm supporting a drive member and wherein the arms are positioned and movable in spaced apart planes above and below the center of gravity of the object stage.

In accordance with another aspect of the present invention, the guideless stage incorporates at least three linear force actuators with two of those actuators driving in one of the X or Y directions and the third actuators driving in the other of the X and Y directions. In accordance with the preferred embodiment of this invention the guideless stage incorporates at least four linear actuators operating between the XY stage and a reaction frame assembly with each actuator including a drive member on the XY stage so that a pair of X drive members serve to drive the XY stage in an X direction and a pair of Y drive members serve to drive the XY stage in the Y direction. The linear actuators and their drive members are constructed, positioned and controlled such that the vector sum of the moments of force at the center of gravity of the XY stage due to the positioning forces of cooperating drive members is substantially equal to zero.

These features and advantages of the present invention will become more apparent upon perusal of the following specification taken in conjunction with the following drawing wherein similar characters of reference refer to similar parts in each of the several views.

Brief Description of the Drawings

Figure 1 is a perspective view of a microlithography system incorporating the present invention.

5 Figure 1A is a view of a portion of the structure shown in Figure 1 delineated by line A-A and with the reaction stage which is shown Figure 1 removed.

Figure 1B is an elevational view, partially in section, of the structure shown in Figure 1.

10 Figure 1C is a schematic elevational view, partially in section, of the object positioning apparatus of the present invention.

Figure 2 is a plan view of the wafer XY stage position above the reaction stage.

15 Figure 3 is a side elevational view of a portion of the structure shown in Figure 2 taken along line 3-3 in the direction of the arrows.

Figure 3A is an enlarged view of a portion of the structure shown in Figure 3 delineated by line B-B.

20 Figure 4 is a perspective view of the reaction stage showing the XY followers without the means for coupling to the XY stage for positioning of the XY stage.

Figure 4A is an enlarged perspective view of the XY followers illustrated in Figure 4.

25 Figure 5 is a schematic block diagram of the position sensing and control system for the preferred embodiment of this invention.

Figures 6 and 7 are views similar to Figures 2 and 3 of an alternative embodiment of the present invention.

30 Figures 8 and 9 are views similar to Figures 2 and 3 of still another embodiment of the present invention.

Figure 10 is an enlarged top view of a portion of the structure shown in Figure 8.

Figure 11 is an end view of the structure shown in Figure 10 taken along line 11-11 in the direction of the arrows.

Detailed Description of the Preferred Embodiment

While it will be appreciated by those skilled in the art that the guideless stage, with or without its isolating reaction frame, has many applications to many different types of instruments for precise positioning of objects, the present invention will be described with respect to a preferred embodiment in the form of a microlithographic instrument for aligning wafers in a system where a lens produces an image which is exposed to the photoresist on the wafer surface. In addition, while the guideless stage with or without its isolation stage can be utilized as a guideless object stage movable in just one direction, such as a X or a Y direction, the preferred embodiment is directed to a guideless XY wafer stage as described below.

Referring now to the drawings, with particular reference to Figs. 1 and 2, there is shown a photolithographic instrument 10 having an upper optical system 12 and a lower wafer support and positioning system 13. The optical system 12 includes an illuminator 14 including a lamp LMP, such as a mercury lamp, and an ellipsoid mirror EM surrounding the lamp LPM. And the illuminator 14 comprises optical integrator such as a fly's eye lens FEL producing secondary light source images and a condenser lens CL for illuminating a reticle (mask) R with uniformed light flux. A mask holder RST holding the mask R is mounted above a lens barrel PL of a projection optical system 16. The lens barrel PL is fixed on a part of a column assembly which is supported on a plurality of rigid arms 18 each mounted on the top portion of an isolation pad or block system 20.

Inertial or seismic blocks 22 are located on the system such as mounted on the arms 18. These blocks 22 can take the form of a cast box which can be filled with sand at the operation site to avoid shipment of a massive structure. An object or wafer stage base 28 is supported from the arms 18 by depending blocks 22 and depending bars 26 and horizontal bars 27 (see Fig. 1A). Fig 1B is an elevational view, partially in section, of the structure shown in Fig 1 except that in Fig. 1B the blocks 22 are shown as being a different configuration than in Figs. 1 and A.

Referring now to Figs. 2 and 3, there are shown plan and elevational views, respectively, of the wafer supporting and positioning apparatus above the object or wafer stage base 28 including the object or wafer or XY stage 30 and the reaction frame assembly 60. The XY stage 30 includes a support plate 32 on which the wafer 34, such as a 12 inch wafer, is supported. The plate 32 is supported in space above the object stage base 28 via vacuum pre-load type air bearings 36 which can be controlled to adjust Z, i.e., tilt roll and focus. Alternatively, this support could employ combinations of magnets and coils.

The XY stage 30 also includes an appropriate element of a magnetic coupling means such as a linear drive motor for aligning the wafer with the lens of the optical system 16 for precisely positioning an image for exposure of a photoresist on the wafer's surface. In the embodiment illustrated, the magnetic coupling means takes the form of a pair of drive members such as X drive coils 42X and 42X' for positioning the XY stage 30 in the X direction and a pair of Y drive members such as drive coils 44Y and 44Y' for positioning the XY stage 30 in the Y direction. The associated portion of the magnetic coupling means on the reaction frame assembly 60 will be described in later detail below.

The XY stage 30 includes a pair of laser mirrors 38X operative with respect to a pair of laser beams 40A/40A' and 38Y operative with respect to a pair of laser beams 40B/40B' of a laser beam interferometer system 92 for determining and controlling the precise XY location of the XY stage relative to a fixed mirror RMX at the lower part of the lens barrel PL of the projection optical system 16.

Referring to Figs. 4 and 4A, the reaction frame assembly 60 has a reaction frame 61 which includes a plurality of support posts 62 which are mounted on the ground or a separate base substantially free from transferring vibrations between itself and the object stage.

The reaction frame 61 includes face plates 64X and 64X' extending between support posts 62 in the X direction and 66Y and

66Y' extending between support posts in the Y direction. Inside the face plates 64-66 a plurality of reaction frame rails 67-69 and 67'-69' are provided for supporting and guiding an X follower 72 and a Y follower 82. Inside face plate 64X are an upper
5 follower guide rail 67 and a lower follower guide rail 68 (not shown) and on the inside surface of the opposite face plate 64X' are upper and lower follower guide rails 67' and 68'. On the inside surfaces of each of the face plates 66Y and 66Y' is a single guide rail 69 and 69', respectively; which is positioned
10 vertically in between the guide rails 67 and 68.

The X follower includes a pair of spaced apart arms 74 and 74' connected at their one end by a cross piece 76. Drive elements such as drive tracks 78 and 78' (see Fig. 2) are mounted on the arms 74 and 74', respectively, for cooperating with the
15 drive elements 42X and 42X' of the XY stage. Since in the illustrated embodiment the drive elements 42X and 42X' on the XY stage are shown as drive coils, the drive tracks on the X follower 72 take the form of magnets. The coupling elements could be reversed so that the coils would be mounted on the X
20 follower and the magnets mounted on the XY stage. As the XY stage is driven in the X and Y direction, the laser interferometer system 92 detects the new position of the XY stage momentarily and generates a position information (X coordinate value). As described in greater detail below with reference to
25 Fig. 5, a servo position control system 94 under control of a host processor (CPU) 96 controls the position of the X follower 72 and the y follower 82 in response to the position information from the interferometer system 92 to follow the XY stage 30 without any connection between the drive coils 42X, 42X' and the tracks 74, 74'.

For movably mounting the X follower 72 on the reaction frame 61, the ends of the arms 74 and 74' at the side of the reaction frame 61 ride or are guided on the rail 69, and the opposite ends of the arms 74 and 74' ride on rail 69' adjacent face plate 66
35 Y'. For moving the X follower 72 a drive member 77 is provided

on the cross piece 76 for cooperating with the reaction frame guide 69 for moving the follower 72 in a direction which is perpendicular to the X direction of the XY stage. Since the precision drive and control takes place in the XY stage 30, the positioning control of the X follower 72 does not have to be as accurate and provide as close tolerances and air gaps as the XY stage 30. Accordingly, the drive mechanism 77 can be made of a combination of a screw shaft rotated by a motor and a nut engaged by the X follower 72 or a combination of a coil assembly and a magnet assembly to establish a linear motor and each combination can be further combined with a roller guiding mechanism.

Similar to the X follower 72, the Y follower 82 includes a pair of arms 84 and 84' connected at their one end by a crossbar 86 and including drive tracks 88 and 88' for cooperating with the Y drive members 44Y and 44Y'. The arms 84 and 84' of the Y follower 82 are guided on separate guide rails. The ends of arm 84 ride or are guided on the upper rails 67 and 67' and the ends of arm 84' are guided on lower rails 68 and 68'. A drive mechanism 87 is provided on the cross piece 86 of the Y follower 82 for moving the Y follower 82 along guides 67, 67', 68 and 68' between the face plates 66Y and 66Y' in a direction perpendicular to the Y direction of the XY stage.

As best illustrated in Fig. 4A, the arms 74 and 74' and crossbar 76' of the X follower 72 all lie within and move in the same plane crossing the Z axis. The center of gravity of the XY stage 30 lies within or is immediately adjacent to this plane. In this construction the drive forces from each of the drive coils 42X and 42X' are in a direction along the length of the arms 74 and 74', respectively. However, the arms 84 and 84' of the Y follower 82 lie within and move in different parallel planes spaced apart along the Z axis from one another respectively above and below and parallel to the plane containing the X follower 72. In the preferred embodiment, the crossbar 86 lies in the lower plane containing the arm 84' and a spacer block 86' is positioned between the overlapping ends of the arm 84 and

crossbar 86 to space the arms 84 and 84' in their respective parallel planes. As with X follower 72, the drive forces from each of the drive coils 44Y and 44Y' are in a direction along the length of the arms 84 and 84'. Also, predetermined gaps in X and Z directions are maintained between the drive coils 44Y(44Y') and the drive tracks 88(88') to achieve the guideless concept.

In operation of the guideless stage and isolated reaction frame of the present invention, the XY stage 30 is positioned in an initial position relative to the projection lens as sensed by the interferometer system 92, and the XY stage 30 is supported in the desired Z direction from the object stage base 28 by the air bearings 36 with the drive coils 42X, 42X', 44Y and 44Y' spaced from the drive elements in the form of drive tracks 78, 78', 88 and 88', respectively. There is no direct contact between the XY stage 30 and the reaction frame 61. That is, there is no path for the vibration of the reaction frame to affect the position of the XY stage and vice versa. There is only indirect contact via the transmission means that deliver the signals to the coils and the laser interferometer position sensing system which then transmits sensed position information to the controller which receives other commands to initiate drive signals which result in movement of the XY stage 30.

With the known position of the XY stage 30 from the interferometer system 92, drive signals are sent from the position control system 94 to the appropriate drive coils, 42X, 42X', 44Y and 44Y' to drive the XY stage to a new desired position. The motion of the XY stage is sensed by the interferometer system 92 and position sensors 98X and 98Y (see Fig. 5), and the X follower 72 and Y follower 82 are driven by the drive members 77 and 87, respectively, to follow the XY stage. As illustrated in Fig. 5, the position sensor 98X detects a variation of the Y direction space between the XY stage 30 and the X follower 72 and generates an electric signal representing the amount of space to the position control system 94. The position control system 94 generates a proper drive signal for

the drive member 77 on the basis of the X position information from the interferometer system 92 and the signal from the position sensor 98X.

Also, the position sensor 98Y detects a variation of X direction space between the XY stage 30 and the Y follower 82 and generates an electric signal representing the amount of space, and the drive member 87 is energized on the basis of the Y position information from the interferometer system 92 and the signal from the position sensor 98Y.

Yaw correction is accomplished by the pairs of linear motors which can be used to hold or offset yaw, or the pairs of linear motors can change the rotational position of the XY stage. The data from either or both pairs of laser beams 40A/40A' and 40B/40B' are used to obtain yaw information. Electronic subtraction of digital position data obtained from measurement using the laser beams 40A and 40A' or 40B and 40B' is performed or both differences are added and divided by two.

This invention allows the positioning function of the XY stage to be accomplished faster than if XY guides were used. Reaction forces created in moving the XY stage can be coupled away from the image forming optics and reticle handling equipment.

This invention needs no precision X or Y guides as compared to a guided stage, and precision assembly and adjustment of the wafer XY stage is reduced due to the lack of precision guides. The servo bandwidth is increased because the linear motor forces in the XY axes act directly on the wafer stage; they do not have to act through a guide system.

Forces from the XY linear motors can all be sent substantially through the center of gravity of the XY stage thereby eliminating unwanted moments of force (torque).

With the X follower 72 and the Y follower 82 mounted and moved totally independently of one another, any vibration of a follower is not conveyed to the wafer XY stage or to the optical system when using commercially available electro-magnetic linear

motors for the magnetic coupling between each of the followers 72 and 82 and the XY stage 30 and with clearance between the coils and magnet drive tracks less than about 1 mm. Additionally, with the arms of one of the followers spaced above and below the arms of the other follower, the vector sum of the moments of force at the center of gravity of the XY stage due to the positioning forces of cooperating drive members is substantially equal to zero.

No connection exists between the XY stage and the follower stages that would allow vibrations to pass between them in the X, Y or θ degrees of freedom. This allows the follower stages to be mounted to a vibrating reference frame without affecting performance of the wafer stage. For example, if the reaction frame were struck by an object, the XY stage and the projection optical system would be unaffected.

It will be appreciated by a person skilled in the art that if the center of gravity is not equidistant between either of the two X drive coils or either of the two Y drive coils, that appropriate signals of differing magnitude would be sent to the respective coils to apply more force to the heavier side of the stage to drive the XY stage to the desired position.

For certain applications the drive elements 42X/42X' or 42Y/42Y' of the actuator or magnetic coupling assembly for supplying electro-magnetic force to the movable XY stage may be held stationary (see Fig. 5) in a static position with respect to movement of the stage in either the X or Y direction, respectively.

In the last of the explanation of this embodiment, referring to Fig. 1C again, the essential structure of the present invention will be described. As illustrated in Fig. 1C, the XY stage 30 is suspended on the flat smooth surface (parallel with the X-Y plane) of the stage base 28 through the air bearings 36 having air discharge ports and vacuum pre-load ports and is movable in X, Y and θ direction on the stage base 28 without any friction.

The stage base 28 is supported on the foundation (or ground, base structure) 21 by the isolation blocks 20, arms 18, blocks 22, the vertical bars 26 and the horizontal bars 27. Each of the isolation blocks 20 is composed of a vibration absorbing assembly to prevent transmission of the vibration from the foundation 21.

Since Fig. 1C is a sectional view of the XY stage 30 along a line through the drive coils 42X, 42X' in Y direction, the following description is restricted about the X follower 72.

In Fig. 1C, the drive coils 42X are disposed in a magnetic field of drive track (magnet array elongated in X direction) 78 mounted on the follower arm 74 and the drive coils 42X' are disposed in a magnetic field of drive track 78' mounted on the follower arm 74'.

The two arms 74, 74' are rigidly assembled to move together in Y direction by the guide rails 69, 69' formed inside of the reaction frame 61. Also, the guide rails 69, 69' restrict the movement of the two arms 74, 74' in X and Z directions. And the reaction frame 61 is directly supported on the foundation 21 by the four support posts 62 independently from the stage base 28.

Therefore, the drive coils 42X(42X') and the drive tracks 78 (78') are disposed with respect to each other to maintain a predetermined gap (a few millimeters) in Y and Z directions.

Accordingly, when the drive coils 42X, 42X' are energized to move the XY stage 30 in X direction, the reaction force generated on the drive tracks 78, 78' is transferred to the foundation 21, not to the XY stage 30.

On the other hand, as the XY stage 30 moves in Y direction, the two arms 74, 74' are moved in Y direction by the drive member 77 such that each of the drive tracks 78, 78' follows respective coils 42X, 42X' to maintain the gap in Y direction on the basis of the measuring signal of the position sensor 98X.

While the present invention has been described with reference to the preferred embodiment having a pair of X drive members or coils 42X and 42X' and a pair of Y drive members or coils 44Y and 44Y', it is possible to construct a guideless stage

and with an isolated reaction frame in accordance with the invention with just three drive members or linear motors such as shown in Figs. 6 and 7. As illustrated in Fig. 6, a pair of Y drive coils 144Y and 144Y' are provided on the stage 130 and a single X drive coil or linear motor 142X is mounted centered at the center of gravity CG' of the XY stage. The Y drive coils 144Y and 144Y' are mounted on the arms 184 and 184' of the Y follower 182, and the X drive coil 144X is mounted on an arm 174" of a X follower 172. By applying appropriate drive signals to the drive coils 142X and 144Y and 144Y', the XY stage can be moved to the desired XY positions.

Referring now to Figs. 8-11, there is shown an alternative embodiment of the present invention which includes links between the XY drive coils 242X, 242X', 244Y and 244Y' and the attachment to the XY stage 30'. These connections include a double flexure assembly 300 connecting the drive coil 244Y to one end of a connecting member 320 and a double flexure assembly 330 connecting the other end of the connecting member 320 to the XY stage 30'. The double flexure assembly 300 includes a flange 302 connected to the coil 244Y. A clamping member 304 is attached via clamping bolts to the flange 302 to clamp therebetween one edge of a horizontal flexible link 306. The other end of the flexible link 306 is clamped between two horizontal members 308 which are in turn integrally connected with a vertical flange 310 to which are bolted a pair of flange members 312 which clamp one edge of a vertical flexible member 314. The opposite edge of the vertical flexible member 314 is clamped between a pair of flange members 316 which are in turn bolted to a flange plate 318 on one end of the connecting member 320. At the other end of the connecting member 320 a plate 348 is connected to two flange members 36 which are bolted together to clamp one end of a vertical flexible member 344. The opposite edge of the vertical member 344 is clamped by flange members 342 which are in turn connected to a plate 340 connected to a pair of clamping plates 338 clamping one edge of a horizontal flexible member 336, the

opposing edge of which is in turn clamped onto the XY stage 30' with the aid of the plate 334. Thus, in each of the double flexure assemblies 300 and 330 vibrations are reduced by providing both a horizontal and a vertical flexible member. In each of these assemblies the vertical flexible members reduce X, Y and θ vibrations and the horizontal flexible members reduce Z, tilt and roll vibrations. Thus, there are eight vertical flex joints for X, Y and θ and eight horizontal flex joints for Z, tilt and roll.

As illustrated in Fig. 11, the coil 244Y is attached to a coil support 245Y which has an upper support plate 246 attached thereto which rides above the top of the magnetic track assembly 288. Vacuum pre-load type air bearings 290 are provided between the coil support 245Y and upper support plate 246 on the one hand and the magnetic track assembly 288 on the other hand.

In an operative example of the embodiment illustrated in Figs. 8-11 the flexible members 306, 314, 344 and 336 are stainless steel 1 1/4" wide, 1/4" long and 0.012" thick with the primary direction of flex being in the direction of the thickness. In the embodiment illustrated members 306 and 314 are mounted in series with their respective primary direction of flex being orthogonal to one another; members 344 and 336 are similarly mounted.

While the present invention has been described in terms of the preferred embodiment, the invention can take many different forms and is only limited by the scope of the following claims.